# **Determination of the efficiency of the BLDC motor based on the analysis of the measured vibrations**



#### **1. Introduction**

BLDC motors find applications in various industries. As referenced in [1, 2], a BLDC motor is a pulse-powered brushless DC motor with electronic commutation. They are widely used in unmanned aerial vehicles, commonly known as drones, for propulsion. Drones incorporate safety features that enable swift response upon detecting a low battery level. During startup, the onboard computer can verify the operational status of all systems, the power supply voltage of the motors, and their proper connection, often indicated by audible signals. Enhancing security can be achieved through various means, one of which involves improving the characteristics of the BLDC motor, as mentioned in [3]. It is possible to measure the motor's current draw while simultaneously gathering information about vibrations, which can provide insights into potential short circuits [4]. Photo-optical sensors, as described in [5], can also be employed. Another approach is to compare the measured characteristics against the specifications provided by the motor manufacturer. Vibrations are typically measured in the time domain, resulting in varying amplitudes. Amidst the vast amount of data that can be challenging to interpret, the Discrete Fourier Transform (DFT) proves to be beneficial, as mentioned in [6, 7, 8]. The Fourier transform allows us to convert the collected data from the time domain to the frequency domain, yielding an amplitude-phase characteristic that is easier to interpret. This test aims to determine the motor's efficiency and compare the obtained results with the theoretical rotational speeds stated by the manufacturer. One notable aspect of this solution is the ability to wirelessly gather data on the technical condition of the motors by measuring vibrations. This feature provides an extra level of security for drone operators.

### **2. Experimental Procedures**

The measurement system comprised of an engine with an attached propeller. The motor under test was a Rocket X2212 with a 950kV rating, indicating 950 revolutions per volt of the supply voltage. Measurements were conducted for constant rotational speeds, ranging from 5% PWM (Pulse Width Modulation) to 100% PWM. Each subsequent measurement increased the power transmitted to the motor by 5% PWM. Vibrations were captured using the LSM303d digital accelerometer, which was connected to the STM32 microcontroller. The microcontroller acted as a data receiver from the sensor and simultaneously converted the received data into the frequency domain. Communication was established via the I2C bus. The transformed data was then transmitted from the STM32 microcontroller to the connected desktop computer using the UART bus. The data files were processed in CSV format, and amplitude-time and amplitude-phase characteristics were plotted in Excel. Finally, the comparison runs were plotted to assess the measured rotational speeds against those specified in the technical documentation of the motor. The second run depicted the recorded deviation level between the measured rotational speeds and the specified values in the documentation.

#### **3. Results and Discussion**

Results can vary due to several factors that influence the actual engine speed. The primary factor is the supply voltage and how the BLDC motor is controlled by the electronic speed controller (ESC). The LSM303d accelerometer is a system that allows for vibration measurements in three perpendicular axes. In the accelerometerengine reference system on the drone's arm, the X and Z axes correspond to vibrations recorded in the horizontal plane, while the Y-axis captures vibrations parallel to the force of gravity. Figure 1 displays the recorded vibrations in the Y-axis as an amplitude-time characteristic for 10% PWM.



**Figure 1.** Amplitude-time characteristics for 10% PWM for a BLDC motor

As depicted in Figure 1, the recorded vibrations appear illegible when attempting to determine the motor speed and efficiency. However, the subsequent step involved utilizing the Discrete Fourier Transform (DFT) to obtain data that enables the plotting of the amplitude-phase characteristic. On the plotted characteristic, distinct peaks known as harmonics of the system become evident. Figure 2 illustrates the amplitude-phase characteristics with identified harmonics corresponding to the engine rotational speed and twice the rotational speed. In the tested engine and propeller system, vibrations are generated with such intensity that, as observed in Figure 2, the desired harmonics can be identified. If the measured vibrations were of lower magnitude, signal filtering techniques such as those described in [9] could be employed. According to [10], the application of Kalman filtering to the Fourier transform is a viable approach. Implementing such enhancements in signal processing would improve the quality of the obtained results.



**Figure 2.** Amplitude-phase characteristics for different engine speeds

rotational speed from the technical documentation, speed deviation.

<b>PWM</b> [%]	<b>Frequency (Hz)</b>	<b>Revolutions (rpm)</b>	<b>Revolutions in</b>	<b>Engine speed</b>
			documentation [rpm]	difference [rpm]
5	8,59	515	599	-84
10	20,51	1231	1197	34
15	30,28	1817	1796	21
20	40,04	2402	2394	8
25	48,84	2930	2993	$-63$
30	56,45	3387	3591	$-204$
35	64,08	3845	4190	$-345$
40	73,78	4427	4788	$-361$
45	82,91	4975	5387	$-412$
50	92,01	5521	5985	$-464$
55	99,08	5945	6584	$-639$
60	107,25	6435	7182	$-747$
65	114,91	6895	7781	-886
70	123,73	7424	8379	$-955$
75	139,88	8393	8978	$-585$
80	151,59	9095	9576	$-481$
85	167,51	10051	10175	$-124$
90	177,28	10637	10773	$-136$
95	182,01	10921	11372	$-451$
100	185,39	11123	11970	$-847$

**Table 1.** Harmonic frequency, revolution per minute from calculation, revolution per minute from documentation and difference between both revolution values

Using the data contained in Table 1, it is possible to determine the characteristics of the rotational speed depending on the PWM signal as Fig. 3. It is possible also plot the ideal characteristic using data from the technical documentation of the BLDC motor as Fig. 4. Based on the

data on the difference in rotational speeds from the measurements and the documentation, the characteristics of the difference in rotations were plotted in Fig. 5.



**Figure 3.** Presentation of the characteristics of determined speed on the PWM value, measurements carried out for the voltage of 12.60 V



**Figure 4.** Ideal and calculated motor speed characteristics for PWM values, measurements carried out at 12.60V



**Figure 5.** Presentation of difference values between revolutions determined by documentation and revolutions determined by measurements

## **4. Conclusions**

Based on the conducted tests and subsequent analysis of the results, the following observations were made:

- 1. The rotational speed of the BLDC motor does not increase linearly with each PWM value. Instead, the speed increment occurs for each subsequent PWM value. At a constant voltage, the motor demonstrates an increase in speed as the PWM values increase.
- 2. The rotational speed error is not constant but varies within the PWM range of 20% to 100%. Notably, a decrease in the error is observed within the PWM range of 70% to 85%, suggesting that the motor exhibits higher efficiency in this range.
- 3. Vibration amplitude reaches its highest values at a PWM of 15%. Further research is required to determine whether this increase is due to system resonance, propeller design, or the material composition of the drone arm.
- 4. In terms of vibration measurements on the X and Z axes, the observed vibrations did not exhibit the same level of repeatability as the measurements on the Y axis. Consequently, it was not possible to identify the harmonic associated with the rotational speed for each PWM value in these axes.

These findings provide valuable insights but may require additional investigation and analysis for a comprehensive understanding of the system's behavior.

### **References**

- [1] J. Przepiórkowski, "Silniki elektryczne w praktyce elektronika", Wydawnictwo BTC, Warszawa 2012.
- [2] A. Dobrowolski, "Elektronika ależ to jest proste", Wydawnictwo BTC, Warszawa 2013
- [3] Y. Park, H. Kim, H. Jang, S. -H. Szynka, J. Lee i D. -H. Jung, "Efficiency Improvement of Permanent Magnet BLDC With Halbach Magnet Array for Drone", w *IEEE Transactions on Applied Superconductivity*, tom. 30, nie 4, s. 1–5, czerwiec 2020, nr art. 5201405, doi: 10.1109/TASC.- 2020.2971672.
- [4] T.A. Shifat and J.W. Hur, "An Effective Stator Fault Diagnosis Framework of BLDC Motor Based on Vibration and Current Signals," in *IEEE Access*, vol. 8, pp. 106968-106981, 2020, doi: 10.1109/ACCESS.2020.3000856.
- [5] K. Kolano, "Zastosowanie czujników foto-optycznych w torze pomiaru prędkości i położenia wirnika silnika BLDC." Przegląd Elektrotechniczny 90.4 (2014): 169–172.
- [6] Lin, Hsiung-Cheng, and Yu-Chen Ye. "Reviews of bearing vibration measurement using fast Fourier transform and enhanced fast Fourier transform algorithms." Advances in Mechanical Engineering 11.1 (2019): 1687814018816751.
- [7] Chioncel, Cristian Paul, et al. "Limits of the discrete Fourier transform in exact identifying of the vibrations frequency." Romanian Journal of Acoustics and Vibration 12.1 (2015): 1
- [8] Lin, Hsiung-Cheng, et al. "Bearing vibration detection and analysis using enhanced fast Fourier transform algorithm." Advances in Mechanical Engineering 8.10 (2016): 1687814016675080.
- [9] Wahab, M. Farooq, F. Gritti, and T.C. O'Haver. "Discrete Fourier transform techniques for noise reduction and digital enhancement of analytical signals." TrAC Trends in Analytical Chemistry 143 (2021): 116354.
- [10] R. Bitmead, A. H. Tsoi, and P. Parker. "A Kalman filtering approach to short-time Fourier analysis." IEEE transactions on acoustics, speech, and signal processing 34.6 (1986): 1493–1501.

# 6